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### Green Electrochemical Ozone Production via Water **Splitting: Mechanism Studies**

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**Abstract:** The green and energy-efficient water splitting reaction using electrocatalysis for O<sub>3</sub> formation provides a very attractive alternative to the conventional energy-intensive cold corona discharge (CCD) method. Among a large number of electrocatalysts explored for the electrochemical ozone production,  $\beta$ -PbO<sub>2</sub> and SnO<sub>2</sub>-based catalysts have proven to be the most efficient ones at room temperature. In this study Density Functional Theory (DFT) calculations have been employed to investigate the possible mechanisms of ozone formation over these two types of catalysts. For both the  $\beta$ -PbO<sub>2</sub> and Ni/Sb-SnO<sub>2</sub> (nickel and antimony doped tin oxide) catalysts the (110) facet was found to be the most stable one. The possible water splitting mechanisms were modeled on both the  $\beta$ -PbO<sub>2</sub> (110) and Ni/Sb-SnO<sub>2</sub> (110) surfaces with particular attention given to the final two reaction steps, the formations of O<sub>2</sub> and  $O_3$ . For the  $\beta$ -Pb $O_2$ , the formation of  $O_3$  was found to occur through an Eley-Rideal style mechanism as opposed to that on the Ni/Sb-SnO<sub>2</sub>, the latter occurs through a Langmuir-Hinshelwood style interaction. Thermodynamic parameters such as the adsorption energies  $(E_{ac})$ , Gibbs free energies  $(\Delta G)$  and activation energies  $(E_{ac})$  have also been obtained, compared and presented, with β-PbO<sub>2</sub> being modelled primarily as solid-liquid phases and Ni/Sb-SnO<sub>2</sub> modelled as gas phase. These DFT findings have provided the basis for a tool to design and develop new electrochemical ozone generation catalysts capable of higher current efficiencies.

Key words: ozone evolution reaction; water splitting; density functional theory; electrocatalysis; surface adsorption and reaction; lead oxide; nickel and antimony doped tin oxide

CLC Number: 0646

The ozone evolution reaction is a fundamental reaction used in water purification employing advanced oxidation processes with ozone (O<sub>3</sub>) as the principal oxidant<sup>[1-5]</sup>. O<sub>3</sub> is the second strongest oxidant behind chlorine (oxidation potential of 2.07 V vs. SHE), with the advantage that it does not produce the same harmful halogenated by-products that chlorine does. Ozone is not only used in water treatment but has a prevalent role in healthcare [6-7], sterilization [8-9] and in chemical synthesis[10]. The current method employed industrially to produce ozone is through the use of a cold corona discharge (CCD) reactor[11-12]. The reactions can be seen below:

$$e + O_2 \rightarrow 2O^{\bullet} + e$$
 (R1)

$$O' + O_2 + M \rightarrow O_3 + M^*$$
 (R2)

$$O' + O_3 \rightarrow 2O_2 \tag{R3}$$

### **Document Code:** A

$$e + O_3 \rightarrow O_2 + O^* + e \tag{R4}$$

In this process a source of dry O<sub>2</sub> is passed through the reactor and reacts with an electron source causing the O<sub>2</sub> atoms to dissociate into two O atoms. These O atoms next interact with O2 molecules that have notbeen dissociated previously forming O<sub>3</sub> as the product. Whilst a relatively simple process in principal, the O<sub>3</sub> formation current efficiencies are reported as low, with the efficiencies of  $2 \sim 12\%^{[11]}$ . Not only this low efficiency, but also the O<sub>3</sub> formed is a gas, making it difficult to be directly applied for aqueous applications such as water treatment due to its difficulty to dissolve once a gas.

In more recent time, a different method has been investigated with the potential to replace this CCD technology. Through the use of electrochemistry/electrocatalysis, the production of  $O_3$  can be achieved with high current efficiencies. The major drawback of this process is the competition between  $O_2$  and  $O_3$  formations with thermodynamics suggesting the formation of  $O_2$  is favoured:

$$O_3 + 6H^+ + 6e \rightarrow 3H_2O E^0 = 1.51 V$$
 (R5)

$$O_2 + 4H^+ + 4e \rightarrow 2H_2O E^0 = 1.23 V$$
 (R6)

As seen from the standard electrode potentials ( $E^0$ ), the formation of  $O_2$  occurs at a lower potential than that for  $O_3$  and therefore will be favoured. In order to promote the formation of  $O_3$ ,  $O_2$  formation must be inhibited. This could be done through the following steps:

- · Suitable catalyst material must be chosen.
- •Material must be chemically and mechanically stable as a very high anodic potential is needed for O<sub>3</sub> formation and then the gas evolution.
- ·Material used must have a high overpotential for oxygen evolution and be resistant to anodic polarization.
- •Additives that partially inhibit the formation of O<sub>2</sub> by blocking the selected active sites may be used.

In order to satisfy these outlined parameters, the careful selection of a catalyst material is required. The literature gives many examples of different systems tested. One of the earliest examples reported employed a platinum catalyst [13-15]. More recently, boron-doped diamond (BDD) [16-17], PbO<sub>2</sub> [18-19] and Ni/Sb/SnO<sub>2</sub> [20-24] catalysts have been preferred as the efficiency values were much greater at room temperature than that of platinum. Of these the  $\beta$ -PbO<sub>2</sub> and Ni/Sb-SnO<sub>2</sub> systems are well studied experimentally and the most efficient, therefore, our initial theoretical study will focus on these two catalysts.

1) Electrochemical Studies on PbO<sub>2</sub> Based Electrodes

In 1982, Foller and Tobias pioneered the study of PbO<sub>2</sub>, with particular emphasis on  $\beta$ -PbO<sub>2</sub><sup>[18]</sup>. Although  $\beta$ -PbO<sub>2</sub> was a superior catalyst in comparison to SnO<sub>2</sub>, platinum and DSA (Dimensionally Stable Anode), it did have some disadvantages associated with it and this must be evaluated:

·Lead is toxic. This is problematic especially

when considered for a water treatment applicationwhere leaching could occur.

·Lead has a short lifetime. The high rates of lead dissolution at high potential have been noted in some cases.

·Lead has a largecurrent efficiency at low temperature with high energy penalty. Although at room temperature the current efficiency is considerably good ( $2 \sim 12\%$ ), however, to achieve larger current efficiency much lower temperatures are needed which incurs a high energy penalty.

In order to compete with CCD reactor technology which does not boast high efficiencies  $(2 \sim 12\%)$ by volume)[11] but does have a relatively long lifetime, the  $\beta$ -PbO<sub>2</sub> anodes can have moderate efficiencies but the anode lifetime must be improved. In 2012, Velichenko et al<sup>[25]</sup>. focused on overcoming the short lifetimes associated with lead oxide anodes. Through the process of electrodeposition, various oxides such as TiO<sub>2</sub> and ZrO<sub>2</sub> were added forming composite materials based on lead oxide. The addition of these oxides was said to have a pronounced effect on the lead oxide structure. After carrying out accelerated life time testing (ALT) it was found that by addition of these oxides and subsequent formation of the composite materials, the lifetime of the anodes increased. At a current density of 200 mA · cm<sup>-2</sup> and 5wt% of TiO<sub>2</sub>, the service life increased from 105 h to 207 h at the same operating conditions. This shows a two-fold increase in service life. The same increase in lifetime was reported for the ZrO<sub>2</sub> case. In 2014, Yao et al. [26] followed on the work carried out by Velichenko on composite lead oxide materials. The preparations of the anodes differ, as Velichenko used direct electrodeposition, whereas Yao used pulse electrodeposi tion. By using pulse deposition the Tan group<sup>[27]</sup> showed that PbO<sub>2</sub> possessed a stronger oxidation stability compared with direct deposition. ALT was again carried out to investigate the stability of the anode with the PbO<sub>2</sub>-ZrO<sub>2</sub> composite electrode having a lifetime 4 times longer than PbO<sub>2</sub>.

In 1998 and 2001, Amadelli and Velichenko<sup>[28-29]</sup> carried out studies on the influence of cations as

dopants. Although many cations have been tested in the past, iron and cobalt have shown the most promising results. The electrodeposition of PbO<sub>2</sub> in the presences of Fe(III) and Co(II) produces a doped material that is stable and has a high electrocatalytic activity for O<sub>3</sub> generation. After running experiments in 1 mol·L<sup>-1</sup> H<sub>2</sub>SO<sub>4</sub>, the O<sub>3</sub> current efficiencies increased from less than 10% using PbO<sub>2</sub> to 20% using Fe-PbO<sub>2</sub> and 12% using Co-PbO<sub>2</sub>. Not only does the doping improves current efficiency values, but provides electrode stability against corrosion, especially in the case of cobalt.

More recently Da Silva et al. [30] continued the initial work by Amadelli and Velichenko, choosing to focus on Fe-PbO<sub>2</sub> as opposed to the cobalt option, as this showed the highest performance between the two. Another study carried out by Rosestolato et al.[31] reports Fe doped anodes showing resistance to corrosion at high anodic potentials, hereby extending the lifetime by decreasing amorphisation of the electrocatalyst. The magnitude to which they increase depends on the individual characteristics such as the level of doping and the electrolyte employed. This is important as the stability of  $\beta$ -PbO<sub>2</sub> electrodes was one of the major problems found in Foller's research. The potential environmental aspect regarding the leaching of lead into the water has also been addressed using a solid polymer electrolyte (SPE) such as Nafion 117<sup>[30]</sup>. This SPE inhibits the solubilisation of Pb<sup>4+</sup> ions and results in reduced leaching into wastewater.

Electrochemical ozone production (EOP) has substantially progressed since the initial work by Foller and Tobias, and the majority of the problems encountered have since been addressed by other groups. Although Foller et al. could generate ozone with current efficiency values of around 10%, the leaching of Pb<sup>4+</sup> ions and short anode lifetime presented major problems. The leaching was by passed by the Da silva and Velichenko groups that employed a SPE, preventing the solubilisation of Pb<sup>4+</sup> ions and so preventing leaching. The issue with short anode lifetime was tackled by the Velichenko and Yao groups, through doping of Fe and Co, and the forma-

tion of composite oxides PbO<sub>2</sub>-ZrO<sub>2</sub> and PbO<sub>2</sub>-TiO<sub>2</sub>.

2) Electrochemical Studies on SnO<sub>2</sub>-Based Electrodes

In 2004 Cheng and co-workers<sup>[32]</sup> reported a new SnO<sub>2</sub> system doped with Sb. Dissolved O<sub>3</sub> was produced from the anode in a UV cell containing 3 mL of 0.1 mol·L<sup>-1</sup> HClO<sub>4</sub>. The Sb-doped SnO<sub>2</sub> electrode was the working electrode that was placed at the bottom of the cell. A 0.8 cm<sup>2</sup> platinum electrode was used as the counter electrode in the upper regions of the cell close to the air. A reference electrode (Ag/AgCl) was placed next to the Sb-doped SnO2. At 2.5 V (vs. Ag/AgCl) a constant potential was applied to the working electrode at room temperature. The concentration of dissolved O3 was monitored by in situ UV spectroscopy at 258 nm with CE values reported to be ~15%. According to Cheng, efficiency values should be higher than quoted as some O<sub>3</sub> was released in the gaseous phase and therefore not accounted for in the efficiency calculations. This was confirmed by the distinct odour that O<sub>3</sub> gave off.

It was later found by Wang and co-workers [22] that the addition of a second dopant to the Sb-SnO<sub>2</sub> system had an effect on the overall performance. The second dopant used was a small amount of nickel. The anode was prepared by doping titanium mesh with nickel, antimony and tin-oxide and pyrolysed at 500 °C. The dip-coating and pyrolysis process were repeated seven times. It was found that the best atomic ratio for these three elements was 1000:16:2 mmol·L<sup>-1</sup> of Sn:Sb:Ni in the precursor solution. The addition of the nickel dopant caused an increase in O<sub>3</sub> generation efficiency to 32.5% at a potential of 2.2 V (vs. Ag/Ag Cl). It should be noted that 0.1 mol·L<sup>-1</sup> H<sub>2</sub>SO<sub>4</sub> was used as the electrolyte in this case. It was clear from the results that the nickel was causing the enhancement in the overall efficiencies; however no reason was given to explain the nickel effect.

Basiriparsa and Abbasi<sup>[20]</sup> presented an explanation to the effect that nickel had on increased current efficiencies. As nickel(III) has a lower valence than tin (IV) andmay act as an electron acceptor, which is capable of introducing positively charged holes in the valence band by accepting electrons from the bulk. The electrons that are donated by antimony(V) and oxygen vacancies could be well compensated with the holes created by nickel(III), leaving the nickel site negatively charged. The negative charge around the nickel site would help to decrease the oxygen adsorption (hence inhibit oxygen evolution reaction). Therefore, after donating electrons, the positively charged antimony(V) sites could be considered Lewis acid sites, in which water was oxidized to OH' free radicals and O2 would hereby form quickly. The O2 formed on the antimony(V) site could then be transferred and adsorbed onto the nickel surface as an intermediate. The adsorbed O2 reacted further with the OH' to form HO3' radical that underwent a quick deprotonation forming O<sub>3</sub>.

Further significant work was carried out by the Christensen and Lin group<sup>[23]</sup> following the procedure employed by Wanget al. but employing a larger anode surface area, a remarkable high current efficiency of 50% was achieved at a cell voltage of 2.7 V. The Ni/Sb-SnO<sub>2</sub> catalysts supported on Ti meshes underwent the dip-coating process for 20 times, with an optimal molar ratio of 3:8:500 for the Ni:Sb:Sn in the precursor solution. The counter electrode was a  $(5 \times$ 5 cm) platinised titanium mesh. Rather than using a small UV cell (containing 3 mL of 0.1 mol·L<sup>-1</sup> HClO<sub>4</sub>) as seen before, this study utilised a large 200 cm<sup>3</sup> cell employing Nafion 117 proton exchange membrane (PEM) to separate anode and cathode in each half of the cell containing an aqueous 0. 5 mol·L<sup>-1</sup> H<sub>2</sub>SO<sub>4</sub> solution. An impressive low running cost, with the electricity usage of only 18 kWh per kg of ozone production, was achieved at room temperature. Furthermore, this system also produces hydrogen at the cathode which can be used as a fuel to feed in a fuel cell to generate electricity, which in turn can be used to offset the electricity cost in the ozone generation.

Concerning the water splitting mechanism for  $\mathrm{O}_3$  production, although discussed by various groups as to the accepted mechanism, there are no literature examples (other than our group) that have investigated the mechanism through the use of density functional

theory (DFT) calculations [33-34]. Considering this, the  $\beta$ -PbO<sub>2</sub> and Ni/Sb-SnO<sub>2</sub> systems were initially chosen to study how the mechanism behaved. In fact  $\beta$ -PbO<sub>2</sub> was one of the first examples of a room temperature electrochemical ozone generation system that showed a greater efficiency than that of the CCD method, and the Ni/Sb-SnO<sub>2</sub> system is the best one in terms of current efficiency. In studying and comparing these two systems it was found that whilst the general mechanism on each catalyst surface could be the same, the surface reactions were found to occur through different modes of adsorption, not to mention the difference in O<sub>2</sub> and O<sub>3</sub> stabilities, and the activation energies for each reaction.

### 1 Theoretical Methods

### 1.1 Density Functional Theory

All density function theory (DFT) calculations were carried out with a periodic slab model using the Vienna Ab-initio simulation programme (VASP)<sup>[35-37]</sup>. A combination of the Generalised Gradient Approximation (GGA) and Perdew-Burke-Ernzernof (PBE) exchange correlation functional was applied<sup>[38]</sup>. The Projector Augmented Wave (PAW) method <sup>[39-40]</sup> was utilized to describe the electron-ion interactions, and the plane wave basis expansion cut-off was set to 500 eV. All adsorption energies where optimized using the force-based conjugate gradient algorithm, whereas the transition states (TS's) were located using the constrained minimization technique<sup>[41-43]</sup>.

In the modelling of both the  $\beta$ -PbO<sub>2</sub> and Ni/Sb-SnO<sub>2</sub> surfaces, a stable facet for each must be determined. Four low index facets, the 100, 110, 111 and 211 arrangements were tested, and in both cases, it was the 110 facet that was deemed most stable. This is analogous to what was seen by Batzill et al. [44] for SnO<sub>2</sub> which is structurally the same as with  $\beta$ -PbO<sub>2</sub>. Both surfaces where modelled as a(2 × 2) unit cell with various surface coverages tested (0. 25 ~ 1 ML). The two-dimensional Brillouin integrations for each were sampled using k-points for the(2 × 2) unit cell using a 3 × 3 × 1 Monkhorst-Pack grid. A four layer slab was employed with the lower two layers fixed and the upper two layers relaxed. Slab separation was

provided normal to the surface by employing a 1.5 nm vacuum region.

Unlike the  $\beta$ -PbO<sub>2</sub> which only has one metal component, the Ni/Sb-SnO<sub>2</sub> surface is made up of three components, the tin, antimony and nickel, and so additional work is required. The SnO<sub>2</sub> (Figure 1A) was first doped with antimony and next the Sb-SnO<sub>2</sub> surface was further doped with nickel. Of the four possible tin atoms on the surface each was replaced with an antimony atom, and then optimized to determine its preferred orientation (Figure 1B). This was repeated for the Ni/Sb-SnO<sub>2</sub> (Figure 1C), with each of the remaining three tin atoms replaced with a nickel atom and again geometry optimization calculations were run with the lower two layers fixed and the upper two layers relaxed. The slab separation would remain at 1.5 nm throughout. All calculations for β-PbO<sub>2</sub>, SnO<sub>2</sub>, Sb-SnO<sub>2</sub> and Ni/Sb-SnO<sub>2</sub> were performed as spin-open.

With regards to the Ni/Sb-SnO<sub>2</sub> surface, the presence of a surface vacancy was also considered. It is a common phenomenon when testing these catalysts using experimental techniques that surface vacancies were detected. For this study an oxygen vacancy at the bridging site was introduced, as this is said to increase the activity at this site by increasing the Lewis acidity.

### 1.2 Surface Adsorption Calculations

The adsorption energy  $(E_{ads})$  of the system was calculated using Equation 1:

$$E_{\text{ads}} = E_{\text{adsorbate on surface}} - E_{\text{surface}} - E_{\text{gas}}$$
 (E1)

where  $E_{\rm adsorbate\ on\ surface}$  is the energy of the adsorbate and the surface,  $E_{\rm surface}$  is the energy of the clean surface and  $E_{\rm gasis}$  the energy of the corresponding adsorbing species in the gas phase. Equation 1 shows that the more negative the adsorption energy is, the greater the adsorption to the surface. Each term in Equation 1 must correspond to the same surface coverage, whether this is a pure metal or metal oxide.

### 2 Results and Discussion

Experimentally, the method for producing O<sub>3</sub> electrochemically has been well studied. However, the exact mechanism by which O<sub>3</sub> formation precedes remains unsolved. It is commonly accepted that the mechanism proceeds via a four-step mechanism involving the splitting of H<sub>2</sub>O to form O<sub>3</sub><sup>[17-18, 45-48]</sup>:

$$H_2O \rightarrow OH^{\bullet}(ads) + H^+ + e$$
 (R7)

$$OH^{\bullet}(ads) \rightarrow O^{\bullet}(ads) + H^{+} + e$$
 (R8)

$$2O(ads) \rightarrow O_2(ads) \rightarrow O_2$$
 (R9)

$$O_2(ads) + O^{\bullet}(ads) \rightarrow O_3(ads) \rightarrow O_3$$
 (R10)

Although each of the four steps is investigated individually, it is Reactions 9 and 10 that are the most in teresting thermodynamically and therefore the majority of the results presented in detail will be concerning these two steps.

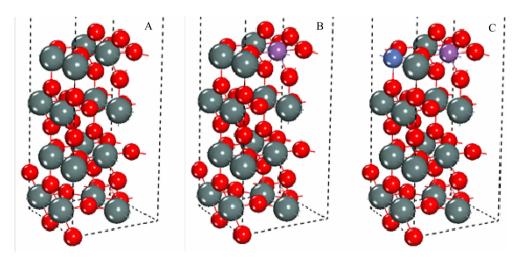


Fig. 1 Models showing the SnO<sub>2</sub>(110) facet (A), the preferred site for antimony doping on the top layer Sb-SnO<sub>2</sub> (B) and the preferred site for further nickel doping on the top layer Ni/Sb-SnO<sub>2</sub> (C)<sup>[34]</sup>. The grey atoms are representative of tin, the purple antimony and the blue nickel.

# 2.1 Ozone Formation Mechanisms over the β-PbO<sub>2</sub> Catalyst

### 2.1.1 Determining the Most Stable Surface Facet of the $\beta$ -PbO<sub>2</sub>

Depending on the crystal structure, a surface arrangement can possess an endless number of facets. These can be categorized as either low-index or high-index facet. For this study low-index facets are preferred as they exhibit atomic smoothness. As no previous studies detail the most stable facet, the 100, 110, 111 and 211 facets were all tested. After geometry optimization of each facet, the 110 derivative was deemed the most stable (Figure 2).

When looking at Figure 2 more closely, it can be seen that the arrangement is analogous to that of rutile  $TiO_2$  and  $SnO_2$ , both well-known metal oxides and therefore the high stability of this (110) derivative is expected.

### 2.1.2 Surface Oxidant Formation and the Construction of a Phase Diagram

It is expected that when carrying out the reaction experimentally the surface of a catalyst will undergo some degrees of oxidation. Structurally, the model

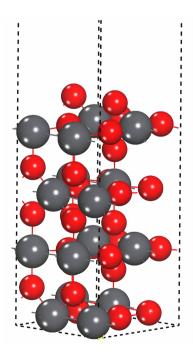


Fig. 2 Model showing the structure of optimized β-PbO<sub>2</sub>(110). The grey atoms represent lead and the red atoms represent oxygen.

shows the surface (or top layer) with four active sites, or four lead atoms with the potential to be oxidized. From Figure 2 it can be seen that two lead atoms reside on the top-sites and two on the bridging sites. As the level of oxidation was not known, the partial coverage and full coverage of the surface were tested. This corresponds to coverages of 0.25, 0.5, 0.75 and 1 mono-layer (ML).

The EOP mechanism shows that the overall oxidation process is the splitting of H<sub>2</sub>O forming O<sub>3</sub>. This coupled with the exposure to the atmosphere would result in OH and O being the main surface oxidants. As well as OH and O, the possibility of surface H<sup>+</sup> must also be accounted for as a proton was lost in Steps 1 and 2 (Reactions R7 and R8 as shown above).

When performing geometry optimization calculations using DFT, the resulting energy is termed the total energy of the system. When constructing a phase diagram the free energy is required. This was calculated using Equation 2:

$$\Delta G = \Delta E + \text{ZPE} - T\Delta S \tag{E2}$$

where  $\Delta E$  is the total energy of the system, the most stable optimized surface; ZPE is the zero-point energy, or the ground state energy; and  $T\Delta S$  is the temperature times the entropy of the system. Although studies have been carried out in both acidic and basic conditions, acidic conditions were favoured and so a pH correction factor was also considered.

After calculating the most stable surface arrangement for all coverages the free energies were calculated and a phase diagram was constructed (Figure 3). Considering the levels of oxidation studied, it was found that 0.5 ML coverage of  $OH_{ads}/O_{ads}$  was closest to that of the experimental potential applied (~1.9 V vs. SHE) and thus preferred.

### 2.1.3 Mechanistic Studies Showing the Formatiion of O<sub>3</sub>

The mechanism proposed by Foller and various other groups shows the formation of  $O_3$  via a series of water spitting reactions (R7 to R10 as shown above), where  $O_2$  was formed prior to the formation of  $O_3$ . This research investigates each of these four steps in dividually with the main emphasis being on Steps 3

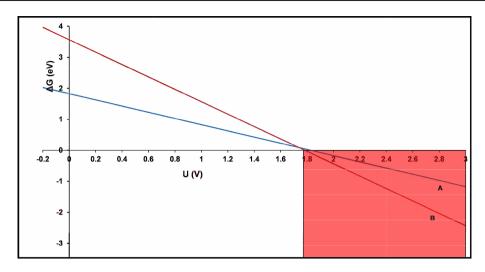


Fig. 3 Plot of  $\Delta G$  of formation of surface oxidants (OH and O) against applied potential (vs. SHE) on the  $\beta$ -PbO<sub>2</sub> (110) surface. The blue line (Line A) represents the stability of adsorbed OH with potential and the red line (Line B) represents the stability of adsorbed O with potential. The white area represents the potential region in which no surface oxidants are present and the red area represents the potential region where the adsorbed OH and O species are formed with O being the predominant surface oxidant.

and 4 (R9 and R10) which are the formations of O<sub>2</sub> and O<sub>3</sub>, respectively.

### 2.1.3.1 Step 1 — The Splitting of H<sub>2</sub>O to Form OH

Step 1 involves the adsorption of  $H_2O$  onto the  $PbO_2$  surface, which is then deprotonated to OH,  $H^+$  and e.

$$H_2O \rightarrow OH^{\bullet}(ads) + H^+ + e$$
 (R7)

When carried out experimentally, the applied potential causes the H<sub>2</sub>O to split at the anode. The OH is left adsorbed at the anode and the H<sup>+</sup> passes through the Nafion membrane to reach at cathode where it is reduced to H then two H combine forming H<sub>2</sub>.

### 2.1.3.2 Step 2 — The deprotonation of OH to form O

In Step 2 the OH adsorbed from Step 1 is deprotonated further to form O and release  $H^{\scriptscriptstyle +}$  and electron.

$$H'(ads) \rightarrow O'(ads) + H'+ e$$
 (R8)

Again by applying a potential, all OH would be deprotonated further to form O. As discussed in the above section 2.1.2, the optimal coverage was found to be 0.5 ML. This would involve the adsorption of 0.5 ML of OH, which is taken from the adsorption of two H<sub>2</sub>O molecules from Step 1 over the unit cell. By deprotonating both the adsorbed OH species, the resulting two O atoms would be ready for Steps 3 and 4, whilst two H<sup>+</sup> would diffuse to cathode where they

would be reduced to form H<sub>2</sub> like in the step 1.

### 2.1.3.3 Step 3— Surface O<sub>2</sub> formation via the interaction of surface O

After Steps 1 and 2, the surface has two O atoms adsorbed on the top sites. These interact with bridging O from the original surface, forming  $O_2$  (ads), with some of this leaving the surface as  $O_2$  (gas).

$$2O'(ads) \rightarrow O_2(ads) \rightarrow O_2$$
 (R9)

In all reactions there would be an initial state (IS), a transition state (TS) and a final state (FS). The IS is deemed the starting point, the TS is the point where the surface adsorbates are highest in energy level and the FS is the product of the reaction. In this case the IS is adsorbed O formed from H<sub>2</sub>O in Step 1, the TS is adsorbed O in close proximity to bridging O but before bond formation and the FS is O<sub>2</sub>(ads). On finding stable geometries for these three states a reaction profile for Step 3 could be constructed (Figure 4).

### 2.1.3.3.1 Initial State of Reaction

The IS of the reaction, as mentioned previously, is two O atoms adsorbed on the top site lead atoms. This corresponds to 0.5 ML coverage of O. The bond distance between the top site and bridging O atoms is 0.2199 nm. The most stable arrangement of the IS has a total energy of -258.95 eV. In the IS shown in

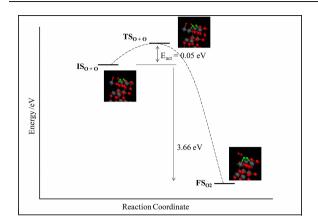


Fig. 4 Energy profile for Step 3 of the mechanism discussed: the formation of surface O<sub>2</sub> from two adsorbed oxygen atoms. The two O atoms highlighted in green are the interacting atoms in the mechanism. The IS shows the adsorbed O and bridging surface O, the TS shows both these two O atoms in a closer proximity to one another, and the FS shows both atoms bonded to form surface O.

Figure 4, the green atoms are the two interacting O atoms.

### 2.1.3.3.2 Transition State of Reaction

The TS is defined as the point which is highest in energy level. In Step 3, the TS is therefore the point in which the two adjacent O atoms (top site and bridging) are closest without bond formation taking place. Locating the TS can often be the most challenging step of the three. By using computational methods, employing the constrained minimization technique discussed earlier, finding the TS is made easier. After determining the most stable arrangement of an adsorbate(s); in this case the O atom, a frequency calculation is run. The distance between the two interacting atoms is fixed, or constrained, and optimized with respects to all remaining degrees of freedom. The bond distance continually changes with each iteration, until the conditions for the TS have been satisfied.

In finding the TS, the activation energy ( $E_{\rm act}$ ) can then be calculated:

$$E_{\text{act}} = E_{\text{TS}} - E_{\text{IS}} = (-258.90) - (-258.95) = 0.05 \text{ eV}$$
(E3)

The  $E_{\rm act}$  was calculated at only 0.05 eV. Thermodynamically the progression from IS to TS would occur

with ease. Both the IS and TS are structurally similar, with bond distance the only difference, hence the favourable minor  $E_{\rm act}$  barrier to overcome.

#### 2.1.3.3.3 Final State of Reaction

The FS of the reaction shows the formation of  $O_2(ads)$ . This occurs via the same top site bridging site interaction shown in the IS. From Figure 4 it can be seen that there is both  $O_2$  adsorbed on the surface and  $O_2$  desorbed. Comparing this observation with what is seen in the literature, this  $O_2(ads)/O_2(gas)$  type state is in agreement with experimental findings. The overall current efficiency values for  $O_3$  formation on  $\beta$ -Pb $O_2$  struggles to reach  $10\%^{[18]}$ . This suggests that for every 100  $O_2$  molecules formed only 10 will remain adsorbed to the surface. The optimized structure for this FS has a total energy of -262.61 eV.

The enthalpy change  $(\Delta H)$  associated with the overall reaction can be calculated using Equation 4:

$$\Delta H = E_{FS} - E_{IS} = (-262.61) - (-258.95) = -3.66 \text{ eV}$$
(E4)

An enthalpy change of -3.66 eV suggests a FS which is very stable in comparison with the IS. The reaction can also be deemed spontaneous and exothermic. To further investigate the stability, the adsorption energy  $(E_{ads})$  for  $O_2$  can be calculated:

$$E_{\text{ads}}(O_2) = E_{\text{(surface }O_2)} - E_{\text{(clean surface)}} - E(O_2) =$$

$$(-252.69) - (-242.77) - (-9.85) = -0.11 \text{ eV (E5)}$$

The adsorption energy was calculated to be-0.11 eV. This suggests a weak adsorption of O<sub>2</sub> to the surface. DFT modelling was carried out in the gas phase, whereas experimentally an acidic aqueous electrolyte is employed<sup>[22]</sup>. Considering this, the reaction itself can be modelled as a liquid phase also. It is assumed from previous work by Kavanagh et al. that the aqueous electrolyte would have a stabilization effect of around -0.30 eV  $^{[49]}\!.$  If this is added to the adsorption of  $O_2$  in the gas phase, the adsorption energy increases to ~ -0.40 eV, making the adsorption much stronger therefore increasing its stability. This method is employed in Step 4 of the model, with the results shown in the next section. This stabilization effect could be explained by the H<sub>2</sub>O/electrolyte solution acting as a cage of hydrogen bonding located above the surface. These interactions cause the  $O_2$  to remain adsorbed for long enough so that  $O_3$  is formed.

2.1.3.4 Step 4— The Association of Surface  $O_2$  and O to Form  $O_3$ 

### 2.1.3.4.1 1st step: The Adsorption of H<sub>2</sub>O

In Step 4 the  $O_2$  formed in Step 3 interacts with surface O to form  $O_3$ . This O atom is obtained by adsorption of  $H_2O$  onto a free lead site adjacent to  $O_2$  (ads).

$$O_2(ads) + O^{\bullet}(ads) \rightarrow O_3(ads) \rightarrow O_3$$
 (R10)  
The H<sub>2</sub>O can be adsorbed on either the top site or bridging region. After calculations the bridging site is deemed more stable; with the  $E_{ads}(H_2O)$  also being calculated using Equation 6:

$$E_{\rm ads}({\rm H_2O}) = E_{\rm (surface\ H_2O)} - E_{\rm (clean\ surface)} - E_{\rm (H_2O)} =$$

$$(-326.49) - (-311.69) - (-14.22) = -0.59\ {\rm eV} \quad (E6)$$
2.1.3.4.2 2<sup>nd</sup> step — The Deprotonation of H<sub>2</sub>O to OH and O

After finding a stable arrangement of  $H_2O$  on the surface, the  $2^{nd}$  step in the formation of surface O can occur. To do this the  $H_2O$  must undergo a double deprotonation. The best way to do this is to carry out each of the deprotonations individually, e.g. deprotonate to OH first, and then to O. After the most stable OH arrangement has been determined, a second deprotonation to O can occur. Each of these deprotonations will have a Gibbs free energy ( $\Delta G_{rxn}$ ) determined by using Equation 7 below:

$$\Delta G_{\text{rxn}} = G(\text{OH}) + G(\text{H}^+ + \text{e}) - G(\text{H}_2\text{O}) =$$

$$(-321.29) + (-3.44) - (-325.90) = 1.17 \text{ eV} \quad (E7)$$

According to the calculated  $\Delta G_{\text{rxn}}$ , a minimum potential of 1.17 V would be required for this deprotonation to occur<sup>[50]</sup>. This is in agreement with the experimental onset which is around 1.80 V or above depending on the relevant conditions.

The second deprotonation will quickly follow as the OH is further deprotonated to surface O. Again the Gibbs free energy ( $\Delta G_{\text{exn}}$ ) was calculated using Equation 7 shown above:

= 
$$(-316.20) + (-3.44) - (-321.29) = 1.65$$
 eV (E8)  
The  $\Delta G_{rxn}$  for this deprotonation was calculated at 1.65 eV. This suggests that a minimum potential of 1.65 V is required for the second deprotonation to

take place. Again this is below the experimental onset of 1.8 V. It should be noted that the second deprotonation requires a higher potential than the first. As a result the second deprotonation is more difficult than the first. This is because that after the first deprotonation, the adsorbate would have changed and as such the potential would change.

2.1.3.4.3 The Formation of O<sub>3</sub> via O and O<sub>2</sub> Coupling Like Step 3, Step 4 would have IS, TS and FS. The IS is O<sub>2</sub>(ads) and O(ads), the TS shows O<sub>2</sub>(ads) and O(ads) in close proximity with one another but before bonding formation, and the FS is O<sub>3</sub>(ads).

#### 2.1.3.4.3.1 Initial State of Reaction

The IS of the reaction involves  $O_2(ads)$  and O(ads). The bond distance between these two is 0.334 nm. The most stable geometry of this IS has a total energy of -316.22 eV.

#### 2.1.3.4.3.2 Transition State of the Reaction

In Step 4, the TS is the point in which the  $O_2$  and O are closest without bond formation taking place. After satisfying the parameters required to determine a suitable TS, the activation energy ( $E_{act}$ ) can be calculated:

$$E_{\text{act}} = E_{\text{TS}} - E_{\text{IS}} = (-315.81) - (-316.22) = 0.41 \text{ eV}$$
 (E9)

The barrier of 0.41 eV suggests that the reaction would precede favourably at room temperature. Considering the value for  $O_2$  adsorption calculated earlier (Eq. 5), it is assumed that this large difference in energy would prevent the reaction with surface O shown in Step 4. The water stabilization effect discussed previously results in the adsorption of  $O_2$  becoming more substantial ( $\sim$  -0.40 eV), thus, increasing the time for surface  $O_2$  to react with surface O before desorption. The current efficiency ( $\sim$  10%) for this system is low, therefore only a small portion of  $O_2$  will stay adsorbed long enough to react and form  $O_3$ .

### 2.1.3.4.3.3 Final State of the Reaction

The FS of the reaction involves the formation of  $O_3$ (ads). This occurs through the coupling of  $O_2$  and O. The enthalpy between the IS and FS can be calculated using Equation 10:

$$\Delta H = E_{\text{FS}} - E_{\text{IS}} = (-316.29) - (-316.22) = -0.07 \text{ eV}$$
(E10)

The  $\Delta H$  change was found to be quite small, -0.07 eV, suggesting a slightly favoured FS (Figure 5). This small difference in energies agrees with the thermodynamics, as  $O_2$  is thermodynamically more stable than  $O_3$ , meaning that the reverse process can occur leading to the decomposition to  $O_2$ .

The  $E_{\rm ads}({\rm O_3})$  was then calculated to determine the strength of adsorption and thus the stability of the  ${\rm O_3}$  molecule:

$$E_{\text{ads}}(O_3) = E_{\text{(surface } O_3)} - E_{\text{(clean surf.)}} - E(O_3) = (-316.29) - (-301.55) - (-13.50) = -1.24 \text{ eV}$$
 (E11)

The value of -1.24 eV suggests a rather strong adsorption to the surface, and so it is likely that the significant amount of surface ozone may not desorb to electrolyte solution then gas phase, but instead may undergo dissociation/decomposition back to O<sub>2</sub>.

When looking more closely at Figure 5, it can be seen that the formation of  $O_3$  occurs on the surface through an Eley-Rideal type mechanism in which the  $O_2$  formed on the surface from Step 3 would desorb and then attack surface O forming  $O_3$  adsorbed on the surface.

# **2.2** Ozone Formation over the Ni/Sb-SnO<sub>2</sub> Catalyst

With regards to the Ni/Sb-SnO<sub>2</sub>, the same four water splitting reaction steps were employed as seen

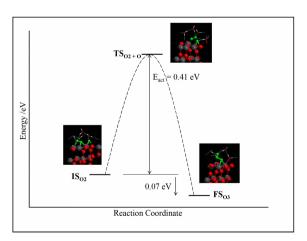


Fig. 5 Energy profile for Step 4 of the mechanism discussed: the transformation from  $O_2$  and O to  $O_3$ . The O atoms highlighted in green are the interacting atoms in the mechanism. The IS shows surface  $O_2$  and O, the TS shows the  $O_2$  desorbed with O still adsorbed, and the FS shows  $O_3$  adsorbed on the surface.

in above section 2.1 on  $\beta$ -PbO<sub>2</sub>. Therefore the calculating of a stable surface facet, the surface phase diagram and the water splitting mechanism for Ni/Sb-SnO<sub>2</sub> catalyst are all discussed in this section. There is conflict in the literature with regards to the water splitting mechanism discussed previously for  $\beta$ -PbO<sub>2</sub>. The majority of literature reports suggest that the formation of O<sub>3</sub> would occur through O<sub>2</sub>H and O<sub>3</sub>H intermediates as opposed to direct O<sub>3</sub> formation. This section will discuss both in detail with a greater emphasis on their direct formation of O<sub>3</sub> as opposed to the intermediate states.

#### 2.2.1 Most Stable Surface Facet

In agreement with the study reported by Batzill et al. [44], the SnO<sub>2</sub>(110) facet was calculated to be the most stable one and thus the doping with Sb and Ni was carried out on this facet (Figure 6A). Batzill et al. also discussed the possibility of surface vacancies or defects, where it was suggested that the SnO<sub>2</sub> was especially susceptible to the presence of an oxygen vacancy (Figure 6B). By creating this vacancy, two cationic Sn sites form which act as Lewis acidic sites and consequently this site tends to be particularly reactive.

Figure 6A shows the most stable arrangement of Ni/Sb-SnO<sub>2</sub>(110), with Sb occupying the bridged region and Ni occupying the top site region. The oxygen vacancy was modelled at different oxygen sites and it was found that the preferred vacancy was the bridged oxygen close to the Sb as shown in Figure 6B.

### 2.2.2 Construction of Phase Diagram for Ni/Sb-SnO<sub>2</sub>

Using the same method shown in section 2.1, a phase diagram (Figure 7) could be constructed for Ni/Sb-SnO<sub>2</sub>. Again the geometry optimization yielded a total energy which was inputted into equation 2 yielding the free energy which in turn could be used to plot a phase diagram. It can be seen clearly from the Figure 7 that adsorbed OH could be formed at potentials above 1.57 V (vs. SHE) and would be the dominant oxidant species whilst O could be formed at potentials above 1.92 V.

After determining the free energies for OH and

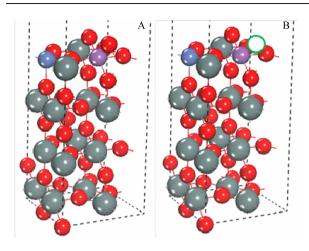


Fig. 6 Models showing the SnO<sub>2</sub> (110) facet doped with Ni and Sb (A) and the same surface but with an oxygen vacancy (B). The grey atoms are Sn, the purple is Sb, the blue is Ni and the green circle represents the vacant site<sup>[34]</sup>.

O, at the selected sub- and mono-layer (ML) coverages, phase diagrams can be constructed. Considering the levels of oxidation studied, it was found that similar to  $\beta$ -PbO<sub>2</sub>, the 0.5 ML coverage was the optimum one as it was formed within the experimental applied potential window for the Ni/Sb-SnO<sub>2</sub> system ( $\sim$  2.7 V).

### 2.2.3 Mechanistic Studies of O<sub>3</sub> Formation over Ni/Sb-SnO<sub>2</sub>(110)

Steps 1 and 2 (reactions R7 and R8) have already been detailed above in section 2.1.3, and as shown in

the phase diagram (Fig. 7) these would occur with ease after a potential (above 1.57 V vs. SHE for step 1 and 1.92 V for step 2) being applied across the surface of anode, therefore the main focus of this section will be the steps 3 and 4, the formation of  $O_2$  and  $O_3$ .

### 2.2.3.1 Step 3 — The Formation of O<sub>2</sub>

The literature reports conflicted theories on how step 3 could occur. It has been suggested that the formation of O<sub>2</sub> could occur via the direct interaction of two O atoms, whereas various groups studying the Ni/Sb-SnO<sub>2</sub> system suggest O<sub>2</sub> formation through the formation of an O<sub>2</sub>H intermediate. These conflicting reactions could be seen below:

$$2O^{\bullet} \rightarrow O_2(ads) \rightarrow O_2(gas)$$
 (R11)

$$2OH^{*} \rightarrow O_2 + 2H^{+} + e$$
 (R12)

Both of these pathways were tested to determine which pathway would be favored. Upon determining the IS, TS and FS of each pathway, energy profiles for all pathways studied were constructed and compared to determine which pathway would be preferred thermodynamically. Reactions 11 and 12 are discussed in two separate sections (2.2.3.2 and 2.2.3.3). 2.2.3.2 The Formation of O<sub>2</sub> via an O<sub>3</sub>H Intermediate

In this section, the formation of  $O_2$  is discussed as going through an OH intermediate as opposed to the direct combination of two O atoms discussed in the next section (2.2.3.3). After  $H_2O$  would has

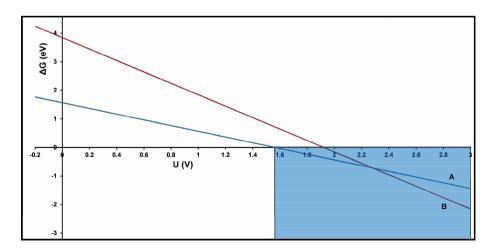


Fig. 7 Plot of  $\Delta G$  of formation of surface oxidants against applied potential (vs. SHE) on the Ni/Sb-SnO<sub>2</sub> surface. The blue line (line A) represents the stability of adsorbed OH with potential and the red line (line B) represents the stability of adsorbed O with potential. The white area represents the potential region in which no surface oxidants are present and the blue area represents the potential region where OH and O could be formed with the OH being the predominant surface oxidant at above 1.57 V.

adsorbed onto the surface and been deprotonated to OH, rather than undergoing further deprotonation, it would interact with O from the surface yielding O<sub>2</sub>H as an intermediate.

The IS of reaction would be adsorbed OH and O, the TS would be where the OH and O being closest before bond formation taking place, the Intermediate (IM) would be the formation of O<sub>2</sub>H and the FS would be the formation of O<sub>2</sub>(ads).

### 2.2.3.2.1 Initial State of Intermediate

The IS in the formation of  $O_2H$  would be OH adsorbed on the top site region and an O atom adsorbed in the surface vacancy reforming the O bridge. The optimized bond distance between the two interacting O and OH was 0.340 nm with a total energy of -301.16 eV.

### 2.2.3.2.2 Transition State of Intermediate

The geometry of the TS was similar to that of the IS, with the OH and O being adsorbed on the surface (Figure 8). The TS was deemed the highest point in energy between the two adsorbates before bond formation occurring. After finding the TS, the activation energy could be calculated using Equation 12:

$$E_{\text{act}} = E_{\text{TS}} - E_{\text{IS}} = (-300.16) - (-301.17) = 1.01 \text{ eV}$$
 (E12)

The  $E_{\rm act}$  was calculated to be 1. 01 eV. In terms of the thermodynamics, the progression from IS to TS would occur slowly, as the higher the barrier is the slower the reaction will occur.

### 2.2.3.2.3 Final State of Intermediate

The FS is the formation of O<sub>2</sub>H in which surface OH and O from the IS interact with each other. The energy associated with this FS was -300.75 eV with the enthalpy calculated using Equation 13:

$$\Delta H = E_{FS} - E_{IS} = (-300.75) - (-301.17) = 0.42 \text{ eV}$$
 (E13)

This enthalpy change of 0.42 eV suggests an endothermic reaction. Figure 8 shows that the FS would be less stable than the IS. In order to be more stable the FS should be lower in energy than the IS. The arrangement of the IS is OH and O, whereas the FS is  $O_2H$ . By comparing both states, the positive change in enthalpy is not surprising, as the IS being made up of OH and O which are well known intermediates that

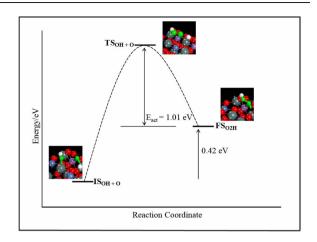


Fig. 8 Energy profile for Step 3 of the mechanism discussed: the formation of an O<sub>2</sub>H intermediate from OH (ads) and O(ads). The O atoms highlighted in green are the interacting atoms in the mechanism. The IS shows the adsorbed OH and O, the TS shows both these atoms in a closer proximity to one another, and the FS shows both atoms bonded to form an O<sub>2</sub>H intermediate.

are relatively more stable than the O<sub>2</sub>H considered in the FS, the latter would be expected to be less stable in comparison.

### 2. 2. 3. 2. 4 The Deprotonation of O<sub>2</sub>H

After the formation of the  $O_2H$  intermediate discussed previously in the above section, the final step of the reaction would be the deprotonation to form  $O_2$ . The difference in energy between these was calculated, and in fact it was simply the energy required to remove a proton from the adsorbate. The energy for the  $O_2H$  as mentioned previously was -300.75 eV and the energy for  $O_2$  was calculated to be -295.48 eV. This gives an energy difference of 5.27 eV which is considered quite large. Upon deprotonating, the adsorption energy ( $E_{ads}$ ) for  $O_2$  (ads) can be determined:

$$E_{\text{ads}}(O_2) = E_{\text{(surface } O_2)} - E_{\text{(clean surface)}} - E(O_2) =$$

$$(-295.59)$$
- $(-284.96)$ - $(-9.85)$ = $-0.78$  eV (E14)

The  $E_{\rm ads}$  was calculated at -0.78 eV. This shows a strong interaction between the surface and the adsorbate, resulting in a stable  $O_2$  adsorbate. After calculating the reaction step shown in Equation 12, a comparison with the direct formation of  $O_2$  was calculated, and is discussed in the next section.

### 2.2.3.3 Direct Formation of O<sub>2</sub> via the Interaction of Two O Atoms

In this case the IS would be two surface adsorbed O atoms, the TS would be the two adsorbed O atoms in closer proximity to one another before bond formation, and the FS would be  $O_2(ads)$ . After calculating stable configurations for each of these three states, an energy profile was constructed (Figure 9).

#### 2.2.3.3.1 Initial State of Reaction

The IS of reaction was two O atoms adsorbed, with one on the top site and the other on the oxygen vacancy site. The bond distance between these two atoms was 0.338 nm. The most stable arrangement had a total energy of -295. 01 eV.

#### 2.2.3.3.2 Transition State of Reaction

The TS of reaction involved the two O atoms from the IS getting closer in energy to one another before bond formation. The progression from IS to TS was deemed the activation energy ( $E_{\rm act}$ ) and was calculated below:

$$E_{\text{act}} = E_{\text{TS}}$$
-  $E_{\text{IS}}$ =(-294.67)- (-295.01)=0. 34 eV (E15)

The  $E_{\text{act}}$  calculated was only 0.34 eV. Thermodynamically the progression from IS to TS should occur with

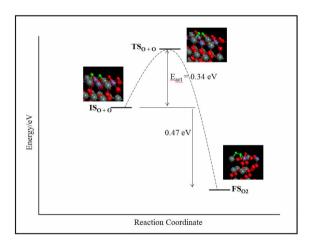


Fig. 9 Energy profile for Step 3 of the mechanism discussed: the formation of surface O<sub>2</sub> from two adsorbed oxygen atoms. The O atoms highlighted in green are the interacting atoms in the mechanism. The IS shows the adsorbed O and bridging surface O, the TS shows both these atoms in a closer proximity to one another, and the FS shows both atoms bonded to form surface O<sub>2</sub><sup>[34]</sup>.

ease. When considering the high potential (2.7 V) used experimentally, this shows further agreement that the reaction would proceed easily.

#### 2.2.3.3.3 Final State of Reaction

The FS of the reaction was the formation of  $O_2$ (ads). This occurred via the interaction of the top site and bridging O atoms from the IS. The geometry or surface arrangement of this  $O_2$  was of particular interest in this step. The different  $O_2$  arrangements tested are shown in Table 1:

Out of these five common surface arrangements, only the bridging and end-on arrangements were deemed suitable as possible FS's for Step 3 as the rest would have desorbed.

Tab. 1 Possible O<sub>2</sub> arrangements and their associated energies

O <sub>2</sub> arrangement	Energy/eV
Bridging	-295.48
Top site	Desorbed
End-on	-295.60
Disigma	Desorbed
Griffiths	Desorbed

The enthalpy for each of these can be calculated using Equation 16, with the data being presented in Table 2:

Tab. 2 The enthalpy changes in both the bridging and end-on geometries

O <sub>2</sub> arrangement	Enthalpy change $(\Delta H)/eV$
Bridging	-0.47
End-on	-0.60

$$\Delta H = E_{\rm FS} - E_{\rm IS} \tag{E16}$$

Table 2 shows that the end-on arrangement was more stable than the bridging analogue, it is, therefore, important to address why the bridging analogue was used. In Step 4, after coupling these two arrange ments with surface O/OH, it was found that the formation of O<sub>3</sub> would only occur through the interac-

tion of bridging  $O_2$  with surface O/OH. In the case of en d-on,  $O_3$  formation does not occur, highlighting that these catalysts could be selective.

An enthalpy of -0. 47 eV for bridging  $O_2$  corresponds to a FS that is more stable in comparison to the IS. The reaction could be deemed spontaneous and exothermic. As  $O_2$  is a stable molecule, the  $E_{ads}$  ( $O_2$ ) can also be calculated:

$$E_{\text{ads}} (O_2) = E_{\text{(surface } O_2)} - E_{\text{(clean surface)}} - E(O_2) =$$
  
(-295.48)- (-284.96)- (-9.85) = -0.68 eV (E17)

The adsorption energy was calculated at -0. 68 eV. This suggests a significant interaction with the surface, further highlighting the stability of  $O_2$ . As the  $E_{act}$  is in fact lower than the adsorption of  $O_2$  (essentially the activation energy for  $O_2$  desorption), the  $O_2$  could remain adsorbed long enough to interact with O(ads) in Step 4 (see below).

### 2. 2. 3. 4 Step 4 — Comparing Pathways for the Formation of O<sub>3</sub>

It is in Step 4 where again like Step 3 the formation of O<sub>3</sub> could occur through either an OH intermediate or an O atom as shown in Reactions 13 and 14:

$$O_2 + O^{\bullet} \rightarrow O_3$$
 (R13)

$$OH' + O_2 \rightarrow O_3H \rightarrow O_3$$
 (R14)

Step 4, the formation of  $O_3$  is the most difficult step in the reaction series.  $O_2$  is thermodynamically more stable than  $O_3$  and the reaction must have a high overpotential for  $O_2$  formation to overcome this thermodynamic barrier. Both Reactions 13 and 14 show different pathways in the formation of  $O_3$ . Section 2.2.3.5 will focus on explaining the results found for Reaction 13 and Section 2.2.3.6 highlights the results found for Reaction 14.

### 2.2.3.5 The Direct Formation of O<sub>3</sub> via the Coupling of O<sub>2</sub> and O

### 2.2.3.5.1 Step 1— The Adsorption of OH

In Step 4,  $O_2$  interacts with O(ads) to form  $O_3$  (Reaction R13). The O is sourced from the adsorption of OH (from electrolyte) and its deprotonation to O.

This OH could be adsorbed on either the top site or bridging region. Upon calculation of both, it was found that the OH preferred to arrange on the top site with a total energy of -304.99 eV as opposed to -304.80 eV when bridged.

After successful adsorption of OH to the surface, the OH must undergo deprotonation to form surface O. With each deprotonation there was a Gibbs free energy ( $\Delta G_{\text{rxn}}$ ) that could be calculated. This was used to determine the minimum applied potential required for the deprotonation to occur:

$$\Delta G_{\text{rxn}} = G(\text{O}) + G(\text{H}^++\text{ e}) - G(\text{OH}) = (-299.18) + (-3.44) - (-304.58) = 1.96 \text{ eV}$$
 (E18)

Equation 18 shows the Gibbs free energy calculated for the deprotonation of OH being 1.96 eV. This suggests that a minimum applied potential of 1.96 V would be required for the second deprotonation to take place. This seems slightly higher than the experimental onset potential, but still well within the electrochemical window of study (2.7 V) for Ni/Sb-SnO<sub>2</sub>. 2.2.3.5.3 Step 3— The Reaction of O<sub>2</sub> (ads) and O (ads) Forming O<sub>3</sub>(ads)

The IS is  $O_2(ads)$  and O(ads), the TS is the point in which  $O_2(ads)$  and O(ads) is highest in energy level before bond formation taking place and the FS is  $O_3$  (ads).

### 2.2.3.5.3.1 Initial State of Reaction

The IS of the reaction is  $O_2$  (ads) and O (ads). The optimized bond distance between these two is 0.335 nm and the total energy of the system is -299.29 eV.

#### 2.2.3.5.3.2 Transition State of Reaction

In this step, the TS would be similar to the IS with  $O_2$  and O both still adsorbed to the surface, with a state that was lower in energy than the IS whilst not being bonded. After calculating a stable geometry for TS the activation energy from IS to TS can be calculated:

$$E_{\text{act}} = E_{\text{TS}}$$
-  $E_{\text{IS}} = (-298.52)$ -  $(-299.29)$ = 0. 77 eV (E19)

Equation 19 shows that the  $E_{\rm act}$  was calculated to be 0.77 eV. This suggests that the reaction would be slow at room temperature, as the higher the  $E_{\rm act}$  the slower the reaction. Taking into consideration that the experimentally applied potential was 2.7 V, this

should drive the reaction to completion. Experimen tally, this reaction was run in aqueous electrolyte, therefore, the water stabilization effect discussed by Kavanagh et al. [49] would lower this barrier further. It should be noted that the activation barrier for gas phase O<sub>3</sub> formation was only slightly higher than the adsorption energy in Step 3 (the energy for desorption of O<sub>2</sub>), if taking the high applied potential and the water stabilizing effect, the barrier would be considerably lower if modelled as a liquid phase reaction, suggesting a feasible process to occur at room temperature.

### 2.2.3.5.3.3 Final State of Reaction

The FS of Step 4 involves the formation of  $O_3$ (ads). This takes place through the coupling of  $O_2$  and O (reaction R13). The enthalpy of reaction from IS to FS can be calculated using equation 20:

$$\Delta H = E_{\text{FS}} - E_{\text{IS}} = (-299.34) - (-299.29) = -0.05 \text{ eV}$$
(E20)

The enthalpy change was only at -0.05 eV, suggesting a slightly more favorable FS (Figure 10). This is not surprising as,  $O_2$  is thermodynamically more stable than  $O_3$ , and therefore the  $O_3$  is likely to decompose back to  $O_2$  and O via the reverse process. This is why a high overpotential is required experimentally for  $O_3$  formation. Through this high overpotential, the  $O_2$  sites would be inhibited and hence promote  $O_3$  formation, therefore stopping this decomposition.

In addition to the  $\Delta H$ , the  $E_{\rm ads}({\rm O_3})$  can be calculated to determine its stability on the surface. This was achieved by measuring the strength of adsorption of  ${\rm O_3}$  to the surface:

$$E_{\text{ads}}(O_3) = E_{\text{(surface } O_3)} - E_{\text{(clean surface)}} - E(O_3) = (-299.34) - (-284.96) - (-13.50) = -0.88 \text{ eV}$$
 (E21)

An  $E_{ads}(O_3)$  value of -0.88 eV suggests a strong ad sorption to the surface and consequently stable adsorption on the surface. However, if the coverage and entropy changes for the adsorption were considered, the value would be reduced to around -0.15 eV at the standard states<sup>[34]</sup>, yielding a much weaker adsorption to the surface.

When looking more closely at Figure 10, it can be seen that the surface mechanism for O<sub>3</sub> formation

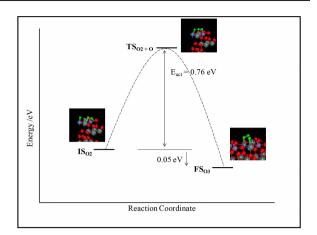


Fig. 10 Energy profile for Step 4 of the mechanism discussed: the transformation from O<sub>2</sub> and O to O<sub>3</sub>. The O atoms highlighted in green are the interacting atoms in the mechanism. The IS shows the O<sub>2</sub> (ads) and O (ads), the TS shows both these atoms in a closer proximity to one another, and the FS shows both atoms bonded to form surface O<sub>3</sub>[34].

occurs through a Langmuir-Hinshelwood interaction in which both  $O_2$  and O are surface adsorbed species. These adsorbed species interact with each other forming  $O_3$  on the surface before desorbing as gaseous  $O_3$ .

### 2.2.3.6 The Formation of O<sub>3</sub> via an O<sub>3</sub>H Intermediate

In this mechanistic step an  $O_3H$  intermediate would be formed before deprotonating to produce  $O_3$ . The rationale for calculating this was to determine whether or not the point at which deprotonation occurs has an effect on the reaction kinetics through calculating the activation barrier of this  $O_3H$  intermediate. Through the adsorption of OH, as discussed in Section 2.2.3.5.1, the surface adsorbates present were  $O_2(ads)$  and OH(ads). Previously, this OH was further deprotonated to O(ads), however, in this case direct interaction of  $O_2$  and OH were tested without deprotonation.

### 2.2.3.6.1 The Interaction of O<sub>2</sub>(ads) and OH(ads) Forming an O<sub>3</sub>H Intermediate

This pathway involves the interaction of  $O_2$ (ads) from Step 3 and OH generated from adsorbed  $H_2O$ . The previously discussed pathway shows the direct formation of  $O_3$  through the deprotonation of OH and subsequent interaction with  $O_2$  forming  $O_3$ . In this

section an attempt was made at carrying out the deprotonation after the interaction of  $O_2$  and OH to form an  $O_3H$  intermediate.

Upon calculation it was found that in each instance the O<sub>3</sub>H dissociated back to OH and O<sub>2</sub>, suggesting that these adsorbates possess a greater stability when compared with O<sub>3</sub>H. Due to the instability of the O<sub>3</sub>H intermediate and the unlikelihood that the reaction would precede via this pathway, no further calculations were carried out. The feasibility of an O<sub>3</sub>H intermediate should be considered by including some experimental parameters (temperature, electrolyte flow rate, potential). However, as these calculations proved extensive and beyond the scope of this paper, they were no longer looked at in detail with regards to this study and further results will be discussed in future publications.

# 2. 3 Catalyst Activity, Selectivity, Lifetime and Regeneration

To develop an efficient catalyst, in addition to high activity and good selectivity, the lifetime must also be considered. For a catalyst to have a long lifetime, it must be able to regenerate itself. This is an area that requires further research with regards to the electrochemical ozone production (EOP) employing the Ni/Sb-SnO2 anodes which have been found to possess a moderate lifetime. Looking at Equation 21, which shows the  $E_{ads}(O_3)$ , it can be seen that the calculated value of adsorption energy for O<sub>3</sub> (at lower coverage, before taking account of coverage and entropy effects) was -0. 88 eV, suggesting a strong adsorption to the surface. This is problematic as in order to increase the lifetime, hereby making the anode regenerable, this adsorbed O<sub>3</sub> must be easily displaced from the surface, freeing up the active sites for continuing EOP. When trying to desorb the O<sub>3</sub> using DFT modelling, it was found that the O<sub>3</sub> preferred to readsorb onto the surface, reaffirming its stability. This finding suggests that practically, we may need to increase the mass transport to remove the produced surface ozone, by employing flowing electrolyte or by increasing the flow rate of circulated electrolyte solution. This DFT study does highlight the reaction

mechanisms, and gives an insight into the reaction barriers and stability of adsorbed species through the calculation of  $E_{\rm act}$  and  $E_{\rm ads}$ . However, more specific experimental factors such as applied potential and flow rate havenot been examined in details within the scope of this study. Nevertheless, O<sub>2</sub> is thermodynamically more stable than O<sub>3</sub>, and therefore, O<sub>3</sub> is likely to decompose back to O2 and O via the reverse process. This is why a high overpotential (e.g., >2.0 V voltage) is required experimentally for O<sub>3</sub> formation. Through this high overpotential, the O<sub>2</sub> sites would be inhibited and hence O<sub>3</sub> formation would promote, therefore, stopping this decomposition and yielding high O<sub>3</sub> selectivity (current efficiency). Although higher voltages will have a positive effect on the O<sub>3</sub> selectivity, the stability of the catalyst may suffer, as a result, the optimum operation voltage (e.g., 2.7 V) is considered suitable to balance both sides in the applications. It should also be noted that this study considers the gas phase reaction, whereas experimentally an aqueous acidic electrolyte is employed. One final thing to be considered is that this study shows the successful formation of a single O<sub>3</sub> molecule on the Ni/Sb-SnO<sub>2</sub>, whereas when run experimentally there may be multiple O2 and O3 molecules along with other OH and O intermediates on the surface at the one time. As a result there will be electrostatic repulsion between the competing adsorbates herein weakening the O<sub>3</sub> adsorption and leading to the successful desorption of O<sub>3</sub>. Taking all of these into account and the high current efficiency (e.g., 50%) values reported, the optimum Ni/Sb-SnO<sub>2</sub> catalyst can clearly represent one that is regenerable and warrants further work to be done both experimentally and theoretically to discover new methods of increasing the overall lifetime.

### 3 Conclusions

The electrochemical ozone production (EOP) via water splitting reactions has attracted increasing interests, thanks to the promising potential of ozone as a green oxidant for many useful applications such as advanced oxidation processes for water treatment, with the most efficient catalysts developed experimentally being  $\beta$ -PbO<sub>2</sub> and Ni/Sb-SnO<sub>2</sub>. Our initial

DFT calculations on these systems, as a first attempt from a theoretical perspective, provided an insight into the complexity of electrocatalysis involved: the preferred surface facet as a function of its stability have been shown, the expected levels of surface oxidation as demonstrated through the construction of phase diagrams, the activation barriers and adsorption energies for O2 and O3 formation revealed that Ni/Sb-SnO<sub>2</sub> catalyst is much more active than  $\beta$ -PbO<sub>2</sub> which explained the experimental results. The final thing of interest was the surface reaction mechanism for the formation of  $O_3$ . On the  $\beta$ -PbO<sub>2</sub> catalyst the formation of O<sub>3</sub> occurs through an Eley-Rideal style mechanism whereas for Ni/Sb-SnO<sub>2</sub> the surface reactions occurred through a Langmuir-Hinshelwood style interaction. This again highlights the complexity associated with the EOP mechanism and as to why more detailed fundamental studies need to be carried out theoretically in understanding the electrocatalysis and more general surface electrochemistry at the quantum level.

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### 绿色电化学水分解法制备臭氧:机理研究

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摘要:采用电催化剂通过水分解反应形成臭氧的绿色节能方法为常规耗能量大的冷电晕放电提供了非常具有吸引力的替代方法.在大量研究的用于电化学合成臭氧的电催化剂中,β-氧化铅(β-PbO<sub>2</sub>)和氧化锡(SnO<sub>2</sub>)基催化剂在室温下最有效.本工作通过密度泛函理论计算,研究了上述两种催化剂作用下臭氧的形成机制.两种催化剂 β-PbO<sub>2</sub> 和镍/锑掺杂氧化锡(Ni/Sb-SnO<sub>2</sub>)的(110)晶面最稳定,故作者特别关注 β-PbO<sub>2</sub>(110)和 Ni/Sb-SnO<sub>2</sub>(110)表面发生的最后两步反应,即氧气和臭氧的形成,模拟了可能的水分解机理.结果表明,在 β-PbO<sub>2</sub> 催化剂的作用下,臭氧是遵循 Eley-Rideal 机理形成,与在 Ni/Sb-SnO<sub>2</sub>表面臭氧的形成机理相反,后者是通过 Langmuir-Hinshelwood 机理形成.将 β-PbO<sub>2</sub> 主要模拟为固-液相,Ni/Sb-SnO<sub>2</sub> 主要模拟为气相,计算得到吸附能(E<sub>ack</sub>)、吉布斯自由能(ΔG)和活化能(E<sub>ack</sub>)等热力学参数值,并进行了分析与比较.这些结果为设计和研发新型的高电流效率电化学制臭氧用催化剂提供了依据.

关键词:臭氧析出反应;水分解;密度泛函理论;电催化;表面吸附和反应;氧化铅;镍/锑掺杂氧化锡